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Polygonal Surface Mesh Optimization

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Abstract

A procedure has been developed to improve polygonal surface mesh quality while maintaining the essential characteristics of the discrete surface. The surface characteristics are preserved by repositioning mesh vertices so that they remain on the original discrete surface. The repositioning is performed in a series of triangular facet-based local parametric spaces. The movement of the mesh vertices is driven by a non-linear numerical optimization process. Two optimization approaches are described, one which improves the quality of elements as much as possible and the other which improves element quality but also keeps the new mesh as close as possible to the original mesh.

Keywords: Polygonal surface mesh, Element quality, Jacobian condition

number, Reference Jacobian Matrices

1 Introduction

This paper describes a procedure to improve the quality of polygonal surface meshes by node repositioning while preserving the essential characteristics of the discrete surface and keeping the mesh close to the original configuration. The need for improvement of such meshes arises primarily in finite volume simulations where they form interior and exterior boundaries of general polyhedral meshes.

While previous research has focused on improving the quality of triangular and quadrilateral meshes [1, 2, 3, 4, 5, 6, 7], little attention has been paid to the improvement of polygonal meshes. Most of this work is devoted to smoothing of a discrete surface represented by polygons (e.g., [8, 9]) rather than improving the quality of the polygonal elements in the surface mesh. In earlier work [10, 7], the authors presented a method for improving the quality of triangular and quadrilateral surface meshes in the absence of an underlying smooth surface. This paper extends and improves this technique to allow smoothing of surface meshes with general polygonal elements.

The rest of the paper is organized as follows. Section 2 describes the minimization of an objective function with respect to local parametric coordinates. The section

discusses the element based local parameterization, line search in local parametric coordinates and moving vertices from one parametric space to another. Section 3 discusses specific objective functions for optimizing the quality of surface meshes. Section 4 presents several examples of optimization of surface meshes to demonstrate the capabilities of the methods.

2 Optimization with respect to Parametric Coordinates

Consider an objective function, $\Psi(\mathbf{x})$, defined in terms of the real coordinates, $\mathbf{x}$, of all the vertices of a surface mesh such that minimization of this function drives the mesh vertices to locations that improve the mesh with respect to some quality measure. If this objective function is minimized directly with respect to the real coordinates of the vertices, the search direction for the minimization may indicate vertex movement off the original surface mesh. To constrain the movement of the vertices to the discrete surface, the optimization must be performed with respect to the coordinates of the vertices in a 2D parametric space corresponding to the surface mesh. Assuming that there is no smooth surface underlying the discrete surface, one of several methods can be used to derive such a global parametric space from the

surface mesh [11, 12, 13, 14, 15]. However, most of these methods involve substantial cost since they require solution of a large system of nonlinear equations.

In this work, instead of using a global parametric space derived from the entire mesh, nodes are repositioned in a series of local parametric spaces. The local parametric spaces are derived from a mapping of mesh edges, and triangular facets of mesh faces to canonical elements in 2D space, as is commonly done in finite element methods. Vertices on the boundary of the surface mesh (i.e., on a model edge) move in parametric spaces of boundary edges of the original mesh. The parametric space of each boundary mesh edge is derived by mapping it to a unit line segment along the X axis giving rise to parametric coordinate $0 \leq s_0 \leq 1$. Vertices in the interior of the surface mesh (i.e., on a model face) move in parametric spaces derived from faces of the original mesh. The parametric space for a mesh triangle is derived using a barycentric mapping [16], resulting in parametric coordinates $0 \leq (s_1, s_2) \leq 1$ (Figure 1a). Quadrilaterals and more general polygons are considered to be made of triangular facets (Figure 1b), and a parametric space is derived for each of them as before. The facetization of polygons is computed by choosing a central point and connecting it to the polygon edges. The central point is chosen by fitting a full quadric

$$Z' = aX'^2 + bX'Y' + cY'^2 + dX' + eY' + f \tag{1}$$

in a rotated frame $\{X', Y', Z'\}$ to the polygon's vertices [17, 18]. If the polygon does not have enough points to fit a full quadric, additional points from the polygon's neighborhood are used.

The optimization procedure keeps track of the facet of the original mesh face that each vertex is moving in. The triangular facet that a vertex is moving in is referred to as the ***base*** triangle. The procedure also keeps track of the coordinates of the vertex in the parametric space of the base triangle. All objective function evaluations are done after mapping the parametric coordinates of the vertex in the base triangle to real coordinates. Also, the line search in the optimization procedure is conducted in the parametric space of the base triangle. The line search is used to find a step size α along a search direction d in the local parametric space while respecting respecting parametric bounds and mesh validity constraints. If an element becomes invalid during a line search, then the step size is scaled back and the optimization restarted along a new search direction. If the line search takes the point out of the parametric bounds of the base triangle, the optimization is stopped, the adjacent triangular facet is found, and the optimization is restarted in the parametric space of the new base triangle. Additional details of the optimization procedure are given in [7].

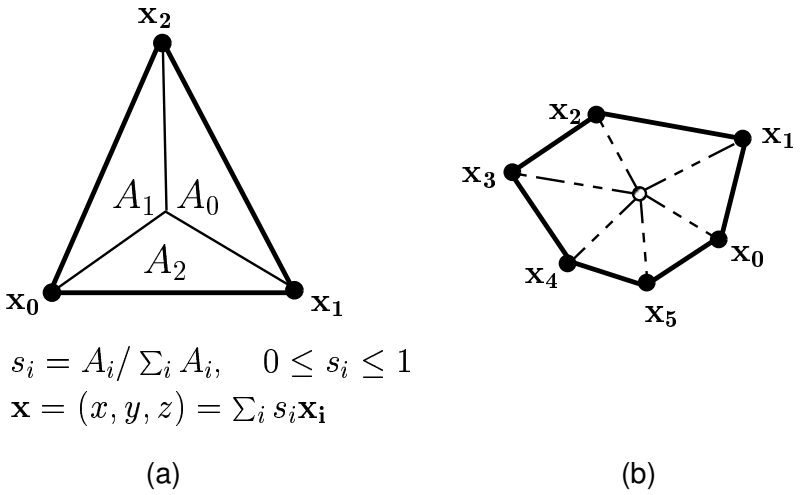


Figure 1: (a) Barycentric mapping for triangle, (b) Triangular facetization of polygon

3 Optimization of Surface Mesh Quality

3.1 Condition Number Shape Measure for Polygonal Mesh Faces

The quality measure used for evaluating the shape of polygonal mesh faces is based on the Condition Number Shape Measure [19]. This measure is derived from the Jacobian matrix of an element mapping as described below.

Consider a vertex V_i, connected to a set of of edges, $\mathcal{E}(V_i)$, and faces, $\mathcal{F}(V_i)$ as shown in Figure 2. Assume that one of the faces $F_j \in \mathcal{F}(V_i)$ has edges $E_p \in \mathcal{E}(V_i)$

and $E_q \in \mathcal{E}(V_i)$ connected to vertex V_i. The triangle formed by edges E_p and E_q can always be mapped to a right triangle in 2D space with V_i mapped to the origin, a unit vector representing E_p along the x-axis and a unit vector representing E_q along the y-axis. Then, the *Jacobian matrix*, $\mathbf{J}_{ji}$, of the mapping of the triangle to the right triangle in 2D space, evaluated at vertex V_i, is given by $\mathbf{J}_{ji} = [\mathbf{e}_p\ \mathbf{e}_q]$ where, $\mathbf{e}_p$ and $\mathbf{e}_q$ are edge vectors representing edges E_p and E_q, of lengths l_p and l_q respectively. The condition number of the Jacobian matrix is defined as $\kappa(\mathbf{J}_{ji}) = |\mathbf{J}_{ji}^{-1}|_F |\mathbf{J}_{ji}|_F$ where $|\cdot|_F$ is the Frobenius norm of its matrix operand.

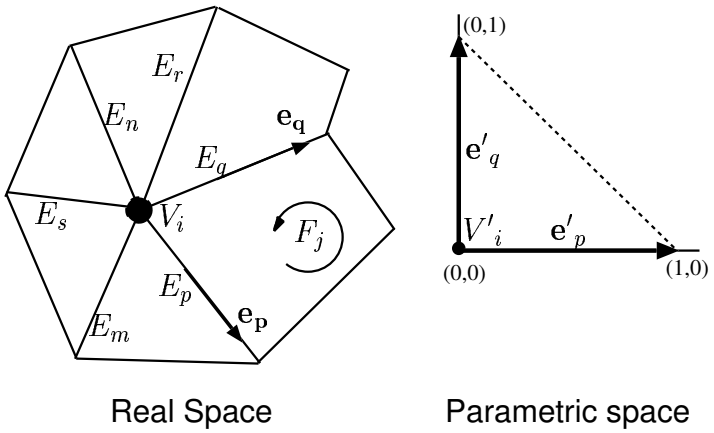


Figure 2: Definition of edge vectors, $\mathbf{e}_p$, $\mathbf{e}_q$ for calculating the Jacobian of an element F_j at vertex V_i.

Since $\mathbf{J}_{ji}$ is a 3x2 matrix for a triangle in 3D, its inverse does not exist in the

usual sense and a pseudo-inverse has to be calculated by singular value decomposition methods. On the other hand, the Jacobian matrix of a triangle in 2D space is a 2x2 matrix whose condition number can be calculated more easily as

$$\kappa(\mathbf{J}_{ji}) = \frac{(l_p^2 + l_q^2)}{2A_j} \tag{2}$$

where A_j is the area of the triangle formed by E_p and E_q [20, 19]. This condition number is only a function of triangle lengths[1]; therefore, it is invariant with rotation of the triangle in the plane. Since there always exists a coordinate system in which an arbitrarily oriented triangle lies on one of its coordinate planes, it suggests that the condition number is also useful for measuring the quality of arbitrarily oriented triangles in space.

The condition number shape measure as described above measures the deviation of an element corner from a right angle corner formed by unit edge vectors. In a given mesh, the quality of any polygonal element is measured by summing the Jacobian condition numbers at the element corners.

[1] A_j is a function of the lengths of the triangle sides

3.2 Condition Number Based Optimization

Consider the minimization of a function defined as the sum of condition numbers of the face corners incident at a given vertex, V_i, as given below:

$$\psi_i^c(\mathbf{x}_i) = \sum_j \kappa(\mathbf{J}_{ji}(\mathbf{x}_i)) = \sum_j \frac{l_p^2(\mathbf{x}_i) + l_q^2(\mathbf{x}_i)}{A_j(\mathbf{x}_i)}, \qquad j \in \{j \mid F_j \in \mathcal{F}(V_i)\} \tag{3}$$

where l_p and l_q are the lengths of the respective edges E_p and E_q of face F_j connected to vertex V_i, and $\mathbf{x}_i$ is the coordinate vector of V_i. Note the presence of area A_j in the denominator as a barrier function which discourages vertex movements that tend to make the triangle formed by E_p and E_q degenerate. Note, however, that it is still important to check explicitly for degeneracy or invalidity of elements in the line search process since it is possible for some line search techniques to jump to the other side of the degeneracy barrier.

The minimization of ψ_i^c attempts to smooth the distribution of face angles and edge lengths around a vertex since all the edge vector pairs are trying to reach equal length and form a right angle. Based on this property, a strategy can be formed for improving the quality of a mesh by minimizing a global condition number based objective function, Ψ^c, defined as:

$$\Psi^c = \sum_i \psi_i^c, \quad i \in \{i \mid V_i \in \mathcal{V}\} \tag{4}$$

where $\mathcal{V}$ is the set of all mesh vertices.

For efficiency reasons, the global function Ψ^c is, in reality, minimized by minimizing a local function, $\widetilde{\psi_i^c}$, at each vertex. $\widetilde{\psi_i^c}$ at a vertex V_i is composed of all terms of Ψ^c that involve the coordinates of V_i. Therefore, $\widetilde{\psi_i^c}$ is formed by visiting each element F_j connected to vertex V_i and adding the Jacobian condition number of the element at V_i and the Jacobian condition numbers at both its edge connected neighbors in that element (See Figure 3). Mathematically, this is written as

$$\widetilde{\psi_i^c} = \sum_j \sum_k \kappa(\mathbf{J}_{jk}),$$

$$j \in \{j \mid F_j \in \mathcal{F}(V_i)\}, \qquad k \in \{k \mid V_k \in \mathcal{V}(F_j) \ \cap \ \mathcal{V}(\mathcal{E}(V_i)) \ \} \tag{5}$$

3.3 Reference Jacobian based Optimization Method

3.3.1 Motivation

The global condition number minimization procedure allows mesh vertices to move along the surface as much as necessary to minimize the objective function, Ψ^c. However, in certain situations, it is of interest to keep the vertices of the original mesh

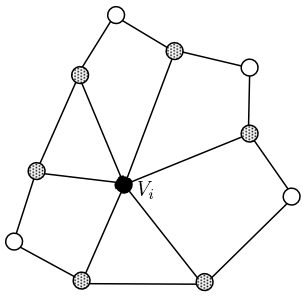


Figure 3: Vertices involved in the local objective function expression, $\widetilde{\psi_i^c}$, for V_i. The shaded circles along with the black circle (V_i) represent the vertices at which the Jacobian is computed for use in $\widetilde{\psi_i^c}$. The white circles represent vertices whose real locations do not contribute to the Jacobian at V_i.

as close as possible to their original locations while improving the shape of the mesh elements. Keeping the vertices close to their original positions facilitates accurate interpolation of solution data from one mesh to another and also preserves mesh characteristics such as refinement and ansiotropy. The *Reference Jacobian Matrix (RJM) based Optimization* [20, 21, 10, 7] is used here to achieve the multiple objectives of improving mesh quality and minimizing the change to the original mesh.

The RJM mesh improvement is a two stage procedure, consisting of a series of local condition number based optimizations and a global RJM optimization as described next.

3.3.2 Local Condition Number based Optimization (Step I)

This is the first stage of the RJM optimization strategy. In this step, the locally optimal position of each mesh vertex is computed with respect to the fixed position of its neighbors. The objective function for optimization is the local condition number function, $\widetilde{\psi_i^c}$, described in Eq. 5, Section 3.2. However, in this step, the vertex is not moved to its locally optimal position. Rather, the optimal position of each vertex, described by a base face and the parametric coordinates of the vertex in the base face, is stored as a virtual position for use in the second stage of the mesh improvement procedure.

3.3.3 Reference Positions, Reference Edges and the Reference Jacobian Matrix

The locally optimal position computed and stored for each vertex in the first stage of the procedure is known as the *reference position* for the vertex. After reference positions are calculated for all mesh vertices, two *reference edge vectors* are calculated for each edge in the mesh; each reference edge vector goes from the reference position of one vertex of the edge to the original position of the other. The idea of reference edges is illustrated in Figure 4, where E_m is an edge with vertices V_a and V_b. The reference positions of V_a and V_b are V_a^R and V_b^R respectively. The two reference edge vectors for E_m are $(\mathbf{e}_m^R)_a$ and $(\mathbf{e}_m^R)_b$, where the outer subscript indicates which of the vertices is at its reference position.

Using the concept of reference edge vectors, it is now possible to define *Reference Jacobian Matrices* (RJMs) just as Jacobian matrices were defined for a mesh without reference positions. Therefore, if the edges of face F_j connected to vertex V_i are E_p and E_q, their reference edges are E_p^R and E_q^R, and their reference edge vectors are $(\mathbf{e}_p^R)_i$ and $\mathbf{e}_q^R)_i$ respectively, then the reference Jacobian of F_j at V_i is defined as $\mathbf{J}_{ji}^R = \left[(\mathbf{e}_p^R)_i \ (\mathbf{e}_q^R)_i\right]$.

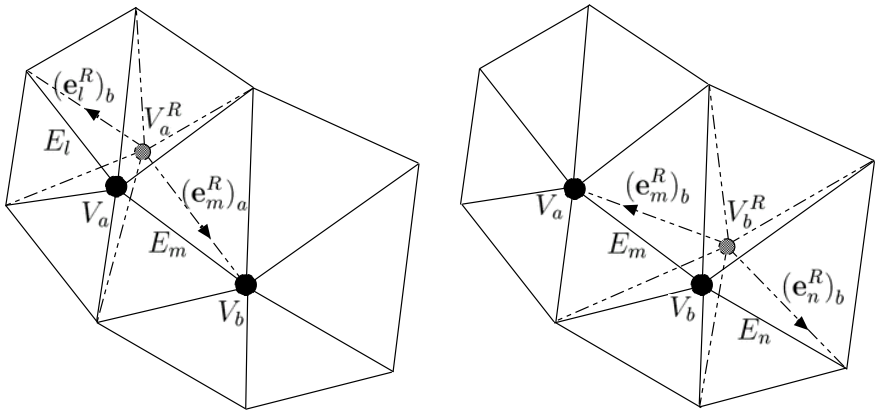


Figure 4: Reference positions and reference edge vectors.

3.3.4 Global Optimization based on Reference Jacobian Matrix (Step II)

The second stage of the mesh improvement procedure is a global optimization based on the definition of reference Jacobian matrices. The goal of this step is to find a valid mesh configuration such that each edge is in a compromise configuration between its pair of reference edges. It is expected that such a configuration for the edges will improve mesh quality, since the reference edge vectors were formed by locally improving mesh quality at each mesh vertex. It is also expected that the optimized mesh will not deviate drastically from the base mesh, since each reference edge vector has one of its vertices at its original position and the other at the locally optimal

position.

The objective function for the global optimization quantifies the difference between the Jacobian matrices of the current mesh configuration and the reference Jacobian matrices as shown below:

$$\Psi^R = \sum_i \sum_j \frac{\left|\mathbf{J}_{ji} - \mathbf{J}_{ji}^R\right|_F^2}{\left|\mathbf{J}_{ji}\right|^2 A_j / A_{ji}^R}, \qquad i \in \{i \mid V_i \in \mathcal{V}\},\ j \in \{j \mid F_j \in \mathcal{F}(V_i)\} \quad (6)$$

where, $\mathcal{V}$ is the set of all mesh vertices, A_{ji}^R is the area of the triangle formed by edge vectors, $(\mathbf{e}_p^R)i$ and $(\mathbf{e}_q^R)i$. Note that, similar to the objective function for local optimization, the objective function includes a barrier term A_j in the denominator in the form of the triangle area to prevent mesh invalidity. Since the Jacobian matrix and the reference Jacobian matrix are formed from the mesh edges and the reference edges respectively, optimization of Ψ^R makes the edges of the final mesh as close as possible to their respective reference edge vectors.

As with the Condition Number based Optimization, the global objective function, Ψ^R is minimized by iteratively minimizing a local component of the global function at each mesh vertex. The local component of the global objective function that involves the real and reference positions of V_i is given as:

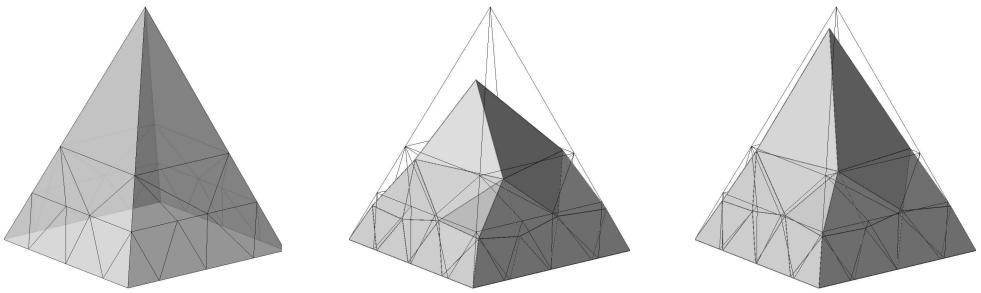
$$\widetilde{\psi_i^R} = \sum_j \sum_k \frac{\|\mathbf{J}_{jk} - \mathbf{J}_{jk}^R\|^2}{|\mathbf{J}_{jk}|^2 A_j / A_{jk}^R},$$

$$j \in \{j \mid F_j \in \mathcal{F}(V_i)\}, \qquad k \in \{k \mid V_k \in \mathcal{V}(F_j) \cap \mathcal{V}(\mathcal{E}(V_i)\}$$

In the expression, the outer sum is over all faces connected to the vertex and the inner sum is over all vertices of a face that include V_i itself or are edge-connected to V_i.

4 Results

Figure 5 shows a simple example to illustrate the effects of a condition number optimization (CN Opt. or CNO) and reference Jacobian based optimization (RJ Opt. or RJO) on a non-planar surface mesh. Figure 5a shows the original pyramid shaped mesh on which the two optimization techniques are applied. Figure 5b shows the effect of optimizing the CN objective function and Figure 5c shows the effect of optimizing the RJ objective function. In both cases, the apex vertex lies on the left lateral surface of the original pyramid. It can be seen that the CN optimization improves the shapes of the triangles more than the RJ optimization. On the other hand, the RJ optimization results in lesser movement of the apex vertex from its original position.



(a) (b) (c)

Figure 5: (a) Original Mesh, (b) Mesh optimized with condition number objective function, (c) Optimized with reference Jacobian objective function. Note that in both cases, the apex vertex is on the lateral surface of the original pyramid.

Figure 6a shows the polygonal mesh of a pig, and Figures 6b and 6c show the results of the CN optimization and RJ optimization on the mesh respectively. It is again clear from the example that the CN optimization improves the shape of mesh elements more than the RJ optimization, but it also causes much more movement of the vertices. In particular, note that the CN optimization destroys much of the anisotropy in the midsection of the pig and smooths away the local refinement around the pig's mouth while the RJ optimization preserves these characteristics of the mesh. Table 1 shows the histograms of the *Normalized Average Condition Number* of elements before and after the two types of optimization. The normalized average condition number for an element is defined as the mean of the condition numbers at

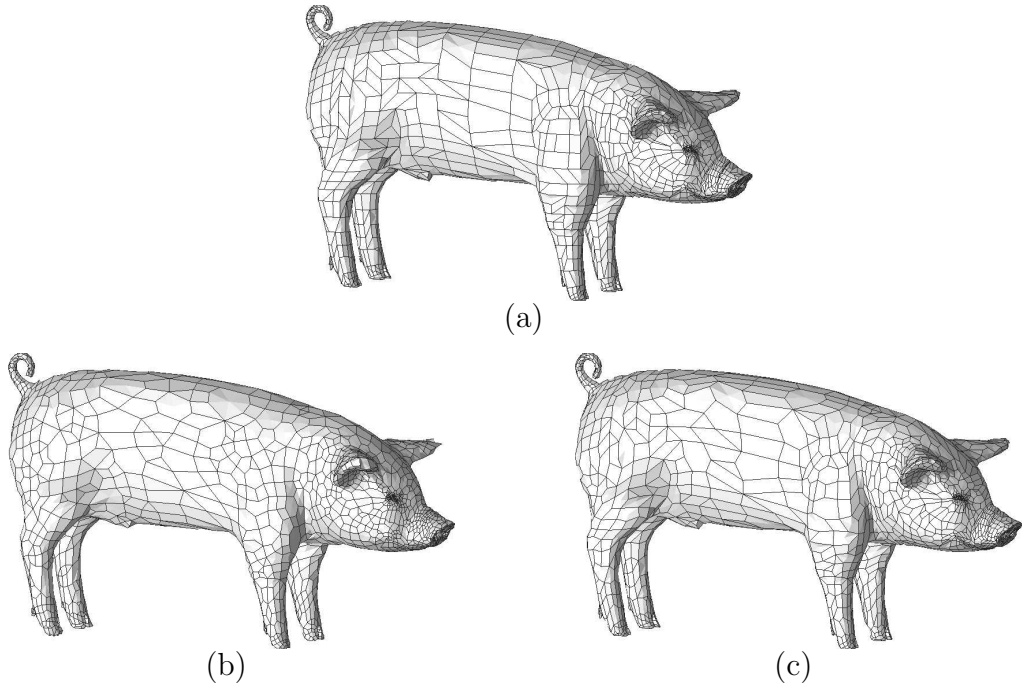


Figure 6: (a) Mesh of pig with anisotropy and local refinement, (b) Mesh optimized with global condition number objective function, (c) Mesh optimized with reference Jacobian objective function.

the vertices of an element, normalized so that a regular polygon will produce a value of 1.

Table 2 shows various quantities computed to measure the change in the meshes and the discrete surfaces using the two methods of optimization. In the table, the normalized Hausdorff distance is computed by finding the minimum distance from each vertex of the original mesh to the new mesh, taking the maximum of these distances [22, 23] and normalizing it by the problem size. The problem size is defined as the maximum length of the domain along the three coordinate directions. The difference between discrete normals is the angle between the normal vector of quadrics fitted to the neighborhood of a vertex at its old and new locations [17, 18]. The maximum vertex movement is the maximum distance traveled by any vertex from its original position and the average vertex movement is the mean of the distance traveled by all vertices from their original positions; these are also normalized by the problem size.

Finally, a complex mesh of a archaelogical artifact is presented in Figure 7 to illustrate the effectiveness of this procedure on large surface meshes. The original mesh for this model was obtained from the Cyberware, Inc.[2] which was then coarsened using software from the Scientific Computation Research Center at Rensselaer

[2] `http://www.cyberware.com/samples`

$\bar{\mathcal{K}}$			Original	CN Opt.	RJ Opt.
1.0	–	1.5	1100	2668	1768
1.5	–	2.0	1017	304	855
2.0	–	3.0	736	49	364
3.0	–	4.0	113	5	31
4.0	–	5.0	25	1	7
5.0	–	7.5	21	0	3
7.5	–	10.0	11	1	0
10.0	–	15.0	3	1	1
15.0	–		3	0	0

Table 1: Histograms of Normalized Average Condition Number of elements in original and optimized polygonal meshes of a pig (Figure 6).

Measure	CN Opt.	RJ Opt.
Hausdorff Distance (% of problem size)	0.3%	0.1%
Ave. Change in Normals	10.7°	4.1°
Max. Vertex Movement (% of problem size)	7.8%	2.6%
Ave. Vertex Movement (% of problem size)	1.0%	0.2%

Table 2: Quantitative measures of the change in the mesh and discrete surface characterics for CN optimization and RJ optimization for polygonal mesh of a pig (Figure 6); distances are presented as a percentage of the problem size.

Polytechnic Institute and then converted into a polygonal mesh. The coarsened mesh (Figure 7a) was used to obtain the optimized meshes shown in the example. A CN optimization resulted in the mesh shown in Figure 7b and a RJ optimization yielded the mesh shown in Figure 7c.

The condition number histograms for the three meshes are presented in Table 3 and the measures for change in surface characteristics are presented in Table 4.

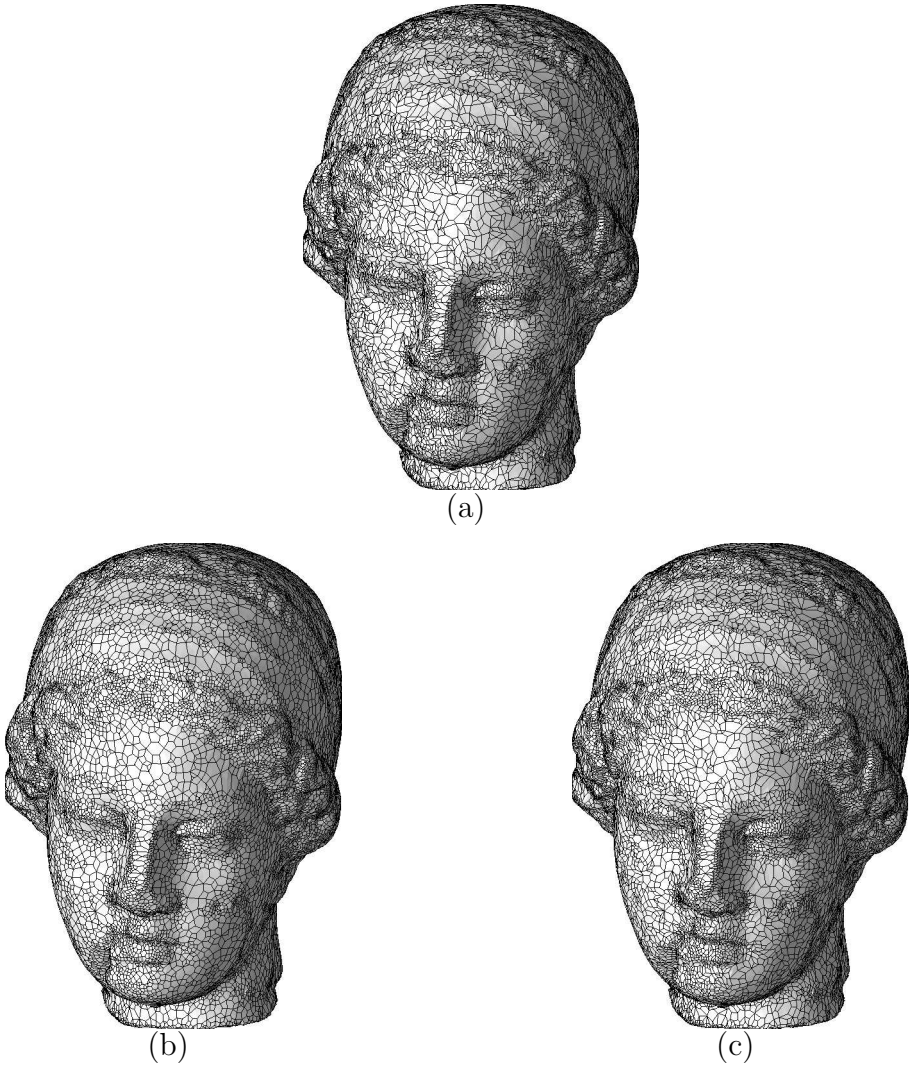


Figure 7: (a) Polygonal mesh of the Igea artifact (from Cyberware, Inc.), (b) Mesh optimized with CN objective function, (c) Mesh optimized with RJ objective function.

$\bar{\mathcal{K}}$			Original	CN Opt.	RJ Opt.
1.0	–	1.5	13135	28117	21899
1.5	–	2.0	10387	892	6500
2.0	–	3.0	5447	47	657
3.0	–	4.0	82	0	0
4.0	–	5.0	1	0	0
5.0	–	7.5	2	0	0
7.5	–	10.0	1	0	0
10.0	–	15.0	1	0	0
15.0	–		0	0	0

Table 3: Histograms of Normalized Average Condition Number in Original and Optimized Meshes for Igea artifact (Figure 7).

Measure	CN Opt.	RJ Opt.
Hausdorff Distance	0.07%	0.07%
Ave. Change in Normals	4.1°	1.5°
Max. Vertex Movement	2.2%	1.0%
Ave. Vertex Movement	0.4%	0.1%

Table 4: Quantitative measures of the change in the mesh and discrete surface characteristics for CN optimization and RJ optimization for Igea artifact (Figure 7); distances are presented as a percentage of the problem size

5 Conclusions

A procedure was presented to improve the quality of complex polygonal surface meshes without an underlying smooth surface using numerical optimization. The optimization is designed to improve the quality of the mesh faces without distorting the discrete surface too much. The vertices are kept on the original surface mesh using movement in local parametric spaces of mesh faces. Two methods were proposed for improving the quality of the surface mesh. The first method improved the quality of mesh elements as much as possible by minimizing a global condition number objective function by local iteration. The second method was the two-stage reference Jacobian

matrix or RJM based method, which improved the mesh quality as well as minimized the movement of vertices from their original locations.

The procedure has been successfully tested on a number of complex triangular and quadrilateral surface meshes. Several quantitative measures were presented to show that both types of optimizations do not distort the surface much.

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References

[1] D. A. Field. Laplacian smoothing and Delaunay triangulations. *Communications in Applied Numerical Methods*, 4:709–712, 1988.

[2] L. Freitag, M. Jones, and P. Plassmann. An efficient parallel algorithm for mesh smoothing. In *Proceedings of the Fourth International Meshing Roundtable*, pages

47–58, Albuquerque, NM, October 1995. Sandia National Laboratories. Sandia Report SAND 95-2130.

[3] P. D. Zavattieri, E. A. Dari, and G. C. Buscaglia. Optimization strategies in unstructured mesh generation. *International Journal of Numerical Methods in Engineering*, 39:2055–2071, 1996.

[4] P. Knupp. Winslow smoothing on two-dimensional unstructured meshes. In *Proceedings of the Seventh International Meshing Roundtable*, pages 449–457, Park City, UT, October 1998. Sandia National Laboratories. Sandia Report SAND 98-2250.

[5] S. A. Cannan, J. R. Tristano, and M. L. Staten. An approach to combined laplacian and optimization-based smoothing for triangular, quadrilateral and quad-dominant meshes. In *Proceedings of the Seventh International Meshing Roundtable*, pages 479–494, Dearborn, MI, October 1998. Sandia National Laboratories. Sandia Report SAND 98-2250.

[6] T. Zhou and K. Shimada. An angle-based approach to two-dimensional mesh smoothing. In *Proceedings of Ninth International Meshing Roundtable*, pages 373–384, New Orleans, CA, October 2000. Sandia National Laboratories. Sandia Report SAND 2000-2207.

[7] R.V. Garimella, M.J. Shashkov, and P.M. Knupp. Triangular and quadrilateral surface mesh quality optimization using local parameterization. *Computer Methods in Applied Mechanics and Engineering*, 2004. To appear.

[8] S Kuriyama. Diffusive smoothing of polygonal meshes with bias and tension control. *The Visual Computer*, 15(10):509–518, 1999.

[9] R.S. Jose, C. Alberola, and J. Ruiz. Reshaping polygonal meshes with smooth normals extracted from ultrasound volume data: An optimization approach. In *Proceedings of SPIE - The International Society for Optical Engineering*, volume 4325, pages 462–472, 2001.

[10] R. V. Garimella, M. J. Shashkov, and P. M. Knupp. Optimization of surface mesh quality using local parameterization. In *Proceedings of the Eleventh International Meshing Roundtable*, pages 41–52, Ithaca, NY, September 2002. Sandia National Laboratories. `http://cnls.lanl.gov/~shashkov`.

[11] K. C. Giannakoglou, P. Chaviaropoulos, and K. D. Papailiou. Boundary-fitted parametrization of unstructured grids on arbitrary surfaces. *Advances in Engineering Software*, 27:41–49, 1996.

[12] M. S. Floater. Parametrization and smooth approximation of surface triangulations. *Computer Aided Geometric Design*, 14:231–250, 1997.

[13] A Sheffer and E de Sturler. Parameterization of faceted surfaces for meshing using angle-based flattening. *Engineering with Computers*, 17(3):326–337, 2001.

[14] M. Desbrun, M. Meyer, and P. Alliez. Intrinsic parameterizations of surface meshes. In *Proceedings of Eurographics 2002 Conference*, Saaebrücken, Germany, September 2002.

[15] I. Guskov. An anisotropic mesh parameterization scheme. In *Proceedings of the Eleventh International Meshing Roundtable*, pages 325–332, Ithaca, NY, September 2002. Sandia National Laboratories.

[16] T. J. R. Hughes. *The Finite Element Method: Linear Static and Dynamic Finite Element Analysis*. Prentice Hall, 1987.

[17] A. M. McIvor and R. J. Valkenburg. A comparison of local surface geometry estimation methods. *Machine Vision and Applications*, 10:17–26, 1997.

[18] S. Petitjean. A survey of methods for recovering quadrics in triangle meshes. *ACM Computing Surveys*, 34(2):211–262, June 2002.

[19] P. M. Knupp. Achieving finite element mesh quality via optimization of the jacobian matrix norm and associated quantitites. Part I - a framework for surface

mesh optimization. *International Journal for Numerical Methods in Engineering*, (48):401–420, 2000.

[20] M. J. Shashkov and P. M. Knupp. Optimization-based reference-matrix rezone strategies for Arbitrary Lagrangian-Eulerian methods on unstructured grids. In *Proceedings of the Tenth Anniversary International Meshing Roundtable*, pages 167–176, Newport Beach, CA, October 2001. Sandia National Laboratories. Sandia Report SAND 2001-2976C.

[21] P. M. Knupp, L. G. Margolin, and M. J. Shashkov. Reference Jacobian optimization-based rezone strategies for Arbitrary Lagrangian Eulerian methods. *Journal of Computational Physics*, 176:93–128, 2002.

[22] P. Cignoni, C. Rocchini, and R. Scopigno. Metro: Measuring error on simplified surfaces. *Computer Graphics Forum*, 17(2):167–174, June 1998.

[23] D. P. Huttenlocher, G. A. Klanderman, and W. J. Rucklidge. Comparing images using the Hausdorff distance. *IEEE Transactions on Pattern Analysis and Machine Intelligence*, 15(3):850–863, September 1993.